

Estimation of Some Thermal Diffusion Parameters by Coupling the Fractional Derivative Theory and the Genetic Algorithm

Rasolomampiany G^{1*}, Rakotoson R², Randimbendrainibe F³

¹Cognitive Sciences and Applications Research Laboratory (LR - SCA), Madagascar

²Doctoral School in Engineering and Innovation Sciences and Techniques (ED - STII), Madagascar

³Ecole Supérieure Polytechnique Antananarivo (ESPA) - University of Antananarivo, BP 1500, Ankatso - Antananarivo 101 – Madagascar

Abstract

This work consists in calculating values of thermal conductivity and the suitable thickness, of a thermal insulator called "thermisorel", by the coupling of the time fractional diffusion equation and the genetic algorithm, taking into account the data and the objectives of the experiment in the article [1].

Keywords: Genetic algorithm • Thermisorel

Introduction

In [1], a heat transfer study was performed on a sample of low density wood fiber board, called Thermisorel. This material is manufactured by STEICO Casteljaloux in France. Thermisorel is used in construction because it prevents heat loss in winter due to their low thermal conductivity, nearly $0.042 \text{ Wm}^{-1} \text{ K}^{-1}$. It also protects the building from heat in summer due to their capacity high thermal storage. In this study, a 22.2 mm thick thermisorel board was used. The details of this study are described [1]. Only the data necessary for our problem mentioned above, which we will recall. This work will be divided into two parts:

In section 2, we will detail the position of our problem, as well as the hypotheses necessary for its resolution. In the third part, we will talk about the genetic algorithm, as well as the time fractional diffusion equation and its discretization in order to give the desired solution

Positioning of the problem

Our problem is to identify suitable optimal values of thermal conductivity and thickness of a thermal insulator, if we vary from 15°C to 24.6°C the temperature of one of the faces and the other will keep a constant temperature of 15° .

To solve this problem, we will use as hypotheses, the data used from the experiment in [1]:

- The density of the insulation: $\rho = 170 \text{ kg.m}^{-3}$

- Specific heat: $C_p = 1280 \text{ J.kg.K}^{-1}$ (according to the measurement made by the CSBT)

- Temperature and heat flux variations as a function of time, on both sides of the thermal insulator plate (see tables below)

***Address for Correspondence:** Rasolomampiany G, Cognitive Sciences and Applications Research Laboratory, BP 1500, Ankatso - Antananarivo 101 – Madagascar, E-mail: rasologil@gmail.com

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From the graphs in [1], we extracted the values of the temperature and those of the flux as a function of time, until the steady state was reached, for the hot side. We have the following tables (Tables 1-3):

Additional assumptions are introduced:

- Since the temperature and the heat flux at any point of each face, at a given time, are identical, then we can restrict the study to a straight segment perpendicular to the two faces, one of the ends of which (noted O) on hot face and the other (noted X) on the face where the temperature is constant

- It is assumed that the variation of the flux, at a given moment, on this segment is linear

The problem thus turns to the following question:

What are the optimal values suitable for thermal conductivity and segment length [O, X]? If the temperature at point O varies according to Table 1-3 during the transient period. And that the temperature of the X end is 15°C during the two regimes, permanent and stationary.

The solution is therefore the values of these two parameters which can give at point X the temperature value closest to 15°C . (If we use the means mentioned at the beginning)

Table 1: Table representation of the temperature variation of the hot face during the transient regime.

| Time in seconds | Temperature in °C |
|-----------------|-------------------|
| 0 | 15 |
| 10 | 15 |
| 20 | 15.67 |
| 30 | 16.34 |
| 40 | 17.34 |
| 50 | 17.5 |
| 60 | 18 |
| 70 | 19 |
| 80 | 20 |
| 90 | 21 |
| 100 | 22.34 |
| 110 | 23.67 |
| 120 | 24.33 |
| 130 | 24.66 |

Table 2: Table representation of the variation of the flux of the hot face during the transient regime.

| Time in seconds | Flux in W .m ⁻² |
|-----------------|----------------------------|
| 0 | 0 |
| 10 | 0 |
| 20 | 18.34 |
| 30 | 20 |
| 40 | 30 |
| 50 | 33.33 |
| 60 | 33.34 |
| 70 | 38.34 |
| 80 | 41.67 |
| 90 | 46.67 |
| 100 | 43.34 |
| 110 | 38.34 |
| 120 | 31.67 |
| 130 | 18.37 |

Table 3: Representation in table form of the variation of the flow of the face where the temperature remains constant during the transient regime.

| Time in seconds | Flux in W .m ⁻² |
|-----------------|----------------------------|
| 0 | 0 |
| 10 | 0 |
| 20 | 0 |
| 30 | 0 |
| 40 | 0 |
| 50 | 0 |
| 60 | 0.77 |
| 70 | 1.54 |
| 80 | 2.31 |
| 90 | 4.62 |
| 100 | 4.62 |
| 110 | 7.69 |
| 120 | 9.23 |
| 130 | 10.77 |

Solution of the Problem by Coupling the Genetic Algorithm and the Fractional Diffusion Equation

The time fractional diffusion equation

In the case of this problem the time fractional diffusion equation is written:

$${}_c D_0^\alpha T(t, x) - a \Delta_x T(t, x) = f(t, x) \tag{1}$$

${}_c D_0^\alpha T(t, x) = \frac{1}{\Gamma(1-\alpha)} \int_0^t (t-\tau)^{-\alpha} T'(\tau, x) d\tau$ is the fractional derivative of

Caputo of order α , $0 < \alpha < 1$ of the variable t , $t > 0$ [2,3]

$t \in [0, T_0]$ and $x \in [0, X]$ with $T_0 = 130$ and X is one of the parameters to be determined and which corresponds to the thickness of the thermal insulator

$a = \frac{k}{\rho C_p}$ is the diffusivity coefficient. k is the other parameter to be determined

$T(t, x)$ is the temperature corresponding to the variables t and x

$f(t, x)$ is the flow corresponding to the variables t and x

For our discretization:

Note that the transient regime stops at the 130th second. Then on the segment $[0, T_0]$

And $[0, X]$, we respectively construct a finite sequence $(t_i)_{0 \leq i \leq 13}$ such that

$l = \frac{T_0}{13}$ and $t_i = il$, a finite sequence $(x_j)_{0 \leq j \leq 13}$ such $h = \frac{X}{13}$ that and

$x_j = jh$

$$\begin{aligned} {}_c D_0^\alpha T(t_i, x_j) &= \frac{1}{\Gamma(1-\alpha)} \int_0^{t_i} (t_i - \tau)^{-\alpha} T'(\tau, x_j) d\tau = \frac{1}{\Gamma(1-\alpha)} \sum_{p=0}^{i-1} \int_{pl}^{(p+1)l} (t_i - \tau)^{-\alpha} T'(\tau, x_j) d\tau \\ &= \frac{1}{\Gamma(1-\alpha)} \sum_{p=0}^{i-1} \int_{pk}^{(p+1)k} T'(t_i - \tau, x_j) \frac{1}{\tau^\alpha} d\tau = \frac{1}{\Gamma(1-\alpha)} \sum_{p=0}^{i-1} \int_{pl}^{(p+1)l} \frac{1}{\tau^\alpha} \frac{T(t_i - pl, x_j) - T(t_i - (p+1)l, x_j)}{l} d\tau \\ &= \frac{1}{\Gamma(1-\alpha)} \sum_{p=0}^{i-1} T(t_i - pl, x_j) - T(t_i - (p+1)l, x_j) \int_{pl}^{(p+1)l} \frac{1}{l \tau^\alpha} d\tau \\ &= \frac{1}{\Gamma(1-\alpha)} \sum_{p=0}^{i-1} T(t_i - pl, x_j) - T(t_i - (p+1)l, x_j) \left[\frac{1}{l} \frac{\tau^{1-\alpha}}{1-\alpha} \right]_{pl}^{(p+1)l} \\ &= \frac{l^{-\alpha}}{(1-\alpha)\Gamma(1-\alpha)} \sum_{p=0}^{i-1} T(t_i - pl, x_j) - T(t_i - (p+1)l, x_j) [(p+1)^{1-\alpha} - p^{1-\alpha}] \\ {}_c D_0^\alpha T(t_i, x_j) &= \frac{l^{-\alpha}}{(1-\alpha)\Gamma(1-\alpha)} \sum_{p=0}^{i-1} T(t_i - pl, x_j) - T(t_i - (p+1)l, x_j) [(p+1)^{1-\alpha} - p^{1-\alpha}] \tag{2} \end{aligned}$$

This relation is valid for $i \neq 0$

For the Laplacian discretization we will use the advanced decentered differentiation [4] and we have:

$$\Delta_x T(t_i, x_j) = \frac{\partial^2}{\partial x^2} T(t_i, x_j) = \frac{T(t_i, x_{j+2}) - 2T(t_i, x_{j+1}) + T(t_i, x_j)}{h^2} \tag{3}$$

The linearity assumption on $f(t, x)$ allows us to write:

$$f(t_i, x_j) = \frac{f(t_i, X) - f(t_i, 0)}{X} x_j + f(t_i, 0) \tag{4}$$

Equation (1) has become:

$$\frac{l^{-\alpha}}{\Gamma(2-\alpha)} \sum_{p=0}^{i-1} (T(t_i - pl, x_j) - T(t_i - (p+1)l, x_j)) [(p+1)^{1-\alpha} - p^{1-\alpha}] - a \frac{T(t_i, x_{j+2}) - 2T(t_i, x_{j+1}) + T(t_i, x_j)}{h^2} = f(t_i, x_j) \tag{5}$$

To simplify the writing, note $T(t_i, x_j) = T_{i,j}$ and $f(t_i, x_j) = f_{i,j}$, hence

$T(t_i - pl, x_j) = T_{i-p,j}$ and the equation (5) has become:

$$\frac{l^{-\alpha}}{\Gamma(2-\alpha)} \sum_{p=0}^{i-1} (T_{i-p,j} - T_{i-(p+1),j}) [(p+1)^{1-\alpha} - p^{1-\alpha}] - a \frac{T_{i,j+2} - 2T_{i,j+1} + T_{i,j}}{h^2} = f_{i,j}$$

We further assume that for $j \geq 13$, $T_{i,j} = T_{i,13}$

For $i = 1$ et $1 \leq j \leq 13$, (5) is written:

$$\begin{aligned} \frac{l^{-\alpha}}{\Gamma(2-\alpha)} (T_{1,j} - T_{0,j}) - a \frac{T_{1,j+2} - 2T_{1,j+1} + T_{1,j}}{h^2} &= f_{1,j} \\ -a \Gamma(2-\alpha) (T_{1,j+2} - 2T_{1,j+1} + T_{1,j}) + h^2 l^{-\alpha} (T_{1,j} - T_{0,j}) &= h^2 \Gamma(2-\alpha) f_{1,j} \\ (1 - \frac{h^2 l^{-\alpha}}{a \Gamma(2-\alpha)}) T_{1,j} - 2T_{1,j+1} + T_{1,j+2} &= -\frac{h^2}{a} f_{1,j} - \frac{h^2 l^{-\alpha}}{a \Gamma(2-\alpha)} T_{0,j} \tag{6} \end{aligned}$$

Specifically

For $i = 1$ and $j = 12$ we have

$$(1 - \frac{h^2 l^{-\alpha}}{a \Gamma(2-\alpha)}) T_{1,12} - T_{1,13} = -\frac{h^2}{a} f_{1,12} - \frac{h^2 l^{-\alpha}}{a \Gamma(2-\alpha)} T_{0,12}$$

For $i=1$ and $j=13$

$$-\frac{h^2 l^{-\alpha}}{a \Gamma(2-\alpha)} T_{1,13} = -\frac{h^2}{a} f_{1,13} - \frac{h^2 l^{-\alpha}}{a \Gamma(2-\alpha)} T_{0,13}$$

For $i=2$ and $1 \leq j \leq 13$

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