

Determination of Pore Size, Porosity and Pore Size Distribution of Woven Structures by Image Analysis Techniques

Ragab A, Fouda A, El-Deeb H and Abou-Taleb H*

Textile Engineering Department, Faculty of Engineering, Mansoura University, Mansoura, Egypt

Abstract

Research Article

Due to the complexity of fabric structure, modeling of pore structure and predicting the pore parameters are difficult. This paper presents a novel approach to determine textile pore size, porosity and pore size distribution by the application of the image analysis techniques. In this study, it has been attempted to establish a theoretical model for both the pore size and porosity of woven fabrics. For this purpose, a theoretical model of porous systems based on Poiseuille's law was used to predict the pore size of woven fabrics. Also a theoretical model was created to predict the porosity of a woven fabric depending on the geometrical parameters. The two characteristics of pore opening size and porosity were determined from image analysis and were compared to the results from laboratory tests. The validity of which was confirmed by experimental results using cotton plain woven fabrics produced from (PSD) determination of woven fabrics is presented in this paper. The tested fabric sample could be ranked in a decrease order successfully.

Keywords: Textile fabrics; Pore size; Porosity pore size distribution; Image analysis; Matlab program

Introduction

Thermal comfort of clothing and textiles is strongly related to fabrics permeability, water-vapour permeability, and waterproofness [1]. On the other hand, these three characteristics are dependent on the porosity and the internal structure [2-4].

The pore properties of the fabric, such as the pore size, pore size distribution, pore shape and porosity, are determined by the fiber and yarn properties and the fabric's structural properties, such as setting and weave type. Accordingly, the prediction of the permeability performance of the fabric used in a certain area can be obtained by the control of the pore properties which have been determined through the fabric's structural properties.

Porosity is defined as the ratio of the total empty area to the total area or as the ratio of the total empty volume to the total volume. The fabric's porosity was introduced as having three different components, which were the inter-fiber and inter yarn porosities; and the effective porosity of the flow that took place in the fabric was described as a function of the inter-fiber and inter-yarn porosities [5].

The introduction of image analysis techniques in textile industry and engineering enhances quality through the efficient use of control [6]. Textile porosity and other related properties, such as air permeability or light transparency, have recently become the focal point of wide and intensive research activity, because of the steadily growing interest on technical textiles and composites [7].

Due to the complex and deformable structure and the non-uniform pore size distribution of textiles, it is somewhat difficult to reach a generalized porosity measure based on measuring the pore dimensions or using the yarn diameter, etc. in order to calculate the air permeability of the fabric [8].

Several studies were oriented to the investigation of the porous structure of woven fabrics [9-11]. Through several studies have treated the pores as cylinders with a permanent cross-section over all its length, the pore size and shape are completely uneven. The same is valid for the pore distribution in the woven fabric [12].

Fewer attempts have been made to determine pore size and its distribution and the fabric structure plays in governing these. The experimental approaches involve a number of disadvantages. They are time-consuming, destructive and lead to inaccurate results since fabrics deform during the procedure.

Therefore, the aim of this study is to present a method, based on image analysis, which is faster, accurate and particularly appropriate for use in measuring porosity, pore size and pore size distribution.

Theoretical Models

Pore size calculation

The proposed model is based on Hagen-Poiseuille equation (1839). For the development of the fabric mathematical model, the following assumptions have been considered:

- a) Threads are uniform along the length.
- b) Threads are equally spaced in the fabric.
- c) There is no flattening in the threads.

The mathematical model presented here is based on the hydraulic radius theory and starts from the first principles of fluid flow. Using Hagen-Poiseuille law for laminar flow through noncircular and irregular in the pore structure and spacing is employed as the following equation [13,14].

$$Q = \frac{R_h^2 \Delta p A_o}{8K \eta \ell}, m^3 / \sec$$
(1)

*Corresponding author: Abou-Taleb H, Textile Engineering Department, Faculty of Engineering, Mansoura University, Mansoura, Egypt, Tel: +20 50 2383781; E-mail: azeemgc7011@gmail.com

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Where Q=Rate of flow through the capillary, Δp =Pressure difference, A_o =Area of the pore space in the channels, η =viscosity of the fluid, *l*=length of the capillary, K=A shape constant that depends on the shape of the pore along the channel (tortuosity) (τ) and orient ration of the pore system and R_h =The hydraulic radius of pore defined as follows [15].

$$R_h = \frac{2A_p}{P_p} \tag{2}$$

Where A_p , P_p and R_h are the area, the wetted perimeter and the hydraulic radius of the pore.

The cross-sectional area of the pores (A_o) in the channels will be $(A\varepsilon)$, where (ε) is the porosity and (A) is the total cross-sectional area. Therefore, Equation (1) can be written as follows:

$$Q = \frac{R_{h}^{2} \Delta p.A\varepsilon}{8K\eta\ell}, \quad m^{3} / \sec$$
(3)

Now if the hydraulic radius (R_h) and the porosity (ε) of both the inter-fibre and inter-yarn flow paths are determined, along with (K), the flow velocity (V) occurring in fabrics can be defined by equation (4):

$$V = \frac{Q}{A} = \frac{dh}{dt} = \frac{\varepsilon R_h^2 \Delta p}{8K\eta h}, m \,/\, \sec$$
(4)

The flow velocity occurring in a capillary tube with a hydraulic radius (Rh) was a function of pressure difference (Equation (4)). The effective forces during the capillary flow occurring in the vertical direction were capillary forces that affected upwarp and gravity forces that affected down. Accordingly, the pressure difference (ΔP) during the capillary flow at a straight capillary tube was defined by Equation (5), described by the Laplace equation as follows [16]:

$$\Delta p = Pc - Pg = \left(\frac{2\gamma\cos\theta}{R_h} - \rho gh\right) \tag{5}$$

In Equation (5), capillary pressure (P_c) was a function of capillary radius (R_h), the contact angle between the fluid surface and the fibre θ and the surface tension of the fluid γ . The gravitational pressure (Pg) depended on the height of the fluid (h), acceleration of gravity (g) and the density of the fluid (ρ). At the equilibrium condition in which the capillary force was equal to gravity force in Equation (5), the maximum capillary rise was reached (Equation 6) at Δp =0.

$$\frac{2\gamma\cos\theta}{R_b} = \rho gh \tag{6}$$

Equation (6) can be rewritten as follows

$$D_h = 2R_h = \frac{2\gamma\cos\theta}{\rho gh} \tag{7}$$

Where D_h=hydraulic pore diameter between yarns, meter

 γ =surface tension energy of the fluid at 23°C, N/m

Cos ($\theta){=}cosine$ contact angle between the fluid surface and the wetted fabric=1

 ρ =the fluid density, kg/m³

g=acceleration of gravity=9.81 m/sec2

h=hydrostatic head pressure, metre.

Surface porosity calculation

Fabric surface porosity (R_s) is defined as the ratio of the total empty area to the total area and can be calculated as follows [17]:

Where, k is cloth cover factor percent

As Figure 1 shows, cloth cover factor percent (k_c) [18,19] can be defined as the percentage of the areas covered by the warp and weft yarns and can be calculated as follows:

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(8)

Cloth cover factor percent (k_c)=(Covered area by yarns/Rectangular area) X 100 (9)

The total rectangular area (ABCD) as shown in Figure 2 can be calculated as $P_1X P_2$.

The area covered by the warp yarn is $d_1X P_2$, and that covered by weft yarn is d_2XP_1 across the material [8].

Therefore, the volume of cloth cover factor percent of the fabric can be calculated as follows:

$$k_{c} = [(P_{1}d_{2} + P_{2}d_{1} - d_{1}d_{2})/P_{1}P_{2}] \times 100, \%$$
(10)

Where k_c is the cloth cover factor percent

 $P_1=1/n1$ (mm), $P_2=1/n2$ (mm) are the distances between two adjacent yarns in the warp and weft directions, and d_1 (mm), d_2 (mm) are the diameters of the warp and weft yarns, respectively.

According to the refs. [20,21], the derived yarn diameter can be obtained as follows:

Which,

$$d = 0.01189 \sqrt{\frac{Den}{0.6pf}}....., mm...$$
(11)

d=yarn diameter in mm







Den=yarn denier and

ρ_f =fiber density, g/cm³

Surface porosity can also be calculated from the projected geometrical area of the opening the percentage of the areas covered by the warp and weft yarns and can be calculated as follows:

$$\varepsilon = \frac{open \ pore \ area}{total \ area} = \frac{P1.P2}{(p1+d1)(p2+d2)} \tag{12}$$

Where

P₁=distance between warp threads

P₂=distance between weft threads

 d_i =diameter of the warp yarn

 d_2 =diameter of the weft yarn.

The main problem in the calculation of porosity is deformation, unevenness and irregular pore size distribution of the textile structures. Neither the distance between yarns nor the diameter of the yarn is uniform; moreover, the thickness is practically never constant across a fabric. Therefore, existing porosity calculation methods that depend on the shape characteristics of the fabric, such as those mentioned earlier in this section, are not useful for estimating the air permeability in practice.

Experimental Work

Fabrics studied

Five samples or raw fabrics of 100% cotton were investigated. The woven samples were tested for their weight and thickness. All of the samples are commercial plain woven.

Image analysis technique

Determination of the pores size and porosity of a woven structure requires a digital camera, personal computer (PC), as well as Matlab program for automatic measurement of the pore size as shown in Figure 2. In this case a digital camera with a resolution of 570 pixels per inch was used. In our research, the measurements taken was mainly of the length. As magnification ratio may change in a test, it was necessary to calibrate length prior to each test.

In this study, 2-D pore size distributions for different fabrics were assessed with assistance of image analysis. Cotton fabrics and indexed with symbols A1, B1, C1, D1, and E1.

The values of parameters of each fabric were determined. The main parameters of the samples are presented in Table 1.

In each sample, picture size was 640X480 pixels and average number of pores per each picture ranges from 342 to 2950 and average number of pores per square centimeter ranges from 50 to 480.

Experimental procedure for measurement of the pore size using image processing method

Four pictures were taken for each sample or 20 fabric images all together. The following steps were performed.

Image acquisition system: A Sony digital camera was used to capture the images of different samples with a resolution of 20X optical zoom as illustrated in Figure 2. The samples were placed over a homogenous white lighting box and the camera was fixed above the samples at a constant distance of 5 cm. Four images for each sample were taken to calculate the average.

The image acquisition system is shown in Figure 2, it includes the personal computer (PC), from grabber, video camera equipped with a zoom lens and system monitor. The fabric image is captured by the video camera, digitized into the video signal with 24-bit gray level resolution and 400×300 pixels by the frame grabber, and stored in frame grabber memory. The fabric is stationary during acquisition, and each image is digitized by a video card into 640×480 pixels with 256 gray levels. Number of pixels per inch for both warp and weft directions are 570. The fabric sample is supplied with light from the back side as shown in Figure 2.

a) Image transmission to Matlab program on a computer: The captured digital images were transferred to computer using Matlab program.

b) Image reading on a Matlab program: Then, the images were read on the Matlab program as RGB images to make a processing on them afterwards.

c) Image converting from RGB to gray: In order to make processing on images, the RGB images were converted into two dimensional gray scale images with 256 gray levels to simplify dealing with them i.e., to improve the computer processing time and speed for the next image processing steps.

An example of this conversion is presented in Figures 3 and 4.

d) Image enhancement: To enhance and process the images, which was done using the Matlab program on a computer, the RGB

Fabric code	Fabric weight (g/m ²)	Fabric *thickness(mm)	Sett (threads/cm)		Yarn count (Den) [Ne]		Air permability **(m ³ / (N.sec))
			warp	weft	warp	weft	
A1 (Black)	122.6	0.4	34	28.8	332.19	332.19	0.000875
					[16 Ne]	[16 Ne]	
B2 (White)	100.8	0.17	35	30	312.65	265.75	0.001025
					[20 Ne]	[17 Ne]	
C3 (Red)	123.5	0.35	29	27	379.64	379.64	0.001125
					[14 Ne]	[14 Ne]	
D4 (Brown)	75.6	0.35	27.6	23.6	88.58	106.3	0.00125
					[15.3 Ne]	[13.3 Ne]	
E5 (Gray)	131.5	0.21	16	12	265.75	379.64	0.002625
					[20 Ne]	[14 Ne]	

**Obtained with the "Shirley" air permeability apparatus, conforming to B.S. Handbook No. 11, P. 308. "Air Permeability of textile Fabrics.

Table 1: Fabric Study.



Figure 3: Image of sample (3) before converting the image from RGB to gray.



Figure 4: Image of sample (3) after converting the image from RGB to gray.



images were converted into gray ones to remove the noise and makes the images more clear.

e) Image conversion from gray to binary: After removing the noise from the images, they will be ready to be converted into black and white images, to be suitable for the next step.

An example of applying this step is presented in Figures 5 and 6.

Object Recognition

A Matlab program was created to recognize the objects in every image. These objects will represent the pore size, pore size distribution and surface porosity in each fabric sample.

Calculating of number of pores and pores area

After recognition the objects in every image, it is now easy to calculate the number of pores using Matlab functions. Also the area of each pore and surface porosity could be calculated. Afterwards, the mean of all areas of pores and the classes of these pore sizes (pore size distribution) were calculated.

Calculating the equivalent pore diameter

After calculating the mean area of the pores (A), an equivalent pore

diameter (de) was calculated for each fabric sample using the following equation:

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$$de = \sqrt{4A/\pi} \tag{13}$$

To complete the necessary information for the virtual model, the shape of the pores has to be determined as well. Either cylindrical or quadratic pore shapes can be chosen. By using the results obtained from the image processing measurement average values of the pore area (A), the equivalent side \mathbf{a}_{eqv} (for square pore shape, (eqn. 14)) or equivalent diameter \mathbf{d}_{eqv} (for circular pore shape, (eqn. 15)) are calculated:

$$a_{eqv} = \sqrt{Aav}$$
(14)

$$d_{eqv} = \sqrt{\frac{4Aav}{\pi}}$$
(15)

The results are present in Figure 7 using Equations (15,17).

Calculating the surface porosity

The most frequently used method for description of the porosity of woven structures is to use the fabric geometry and its parameters like count of the warp and weft yarns (or their diameter), yarn density in warp and weft direction (yarn density), etc. Therefore, the permeability of a single textile layer can be theoretically and experimentally expressed via its porosity (or structure of the porous medium), using parameters like average pore size, number of pores, etc. [12,22,23].

Xu and Wang (2005) [22] and Ogulata (2006) [23] used the following equation for calculation of the area (A) of a pore:

$$\mathbf{A} = \left(\frac{100}{n1} - dI\right) \left(\frac{100}{n2} - d2\right), mm^2$$
(16)

Where d_1 , d_2 are the average diameters of warp and weft threads,





Figure 7: A photograph of the equivalent pore diameter apparatus.

(mm) respectively; n_1 is the warp density (ends/dm), and n_2 is the weft density (picks/dm).

Equivalent Pore Diameter Measurement Traditionally (de)

A photograph of the apparatus used is shown in Figure 5 and the main features of the apparatus are shown in Figure 6 and ref. [24]. The specimen holder consists essentially of a brass cylindrical vessel (l) over which the specimen (2) is clamped by a clamping ring (3) and screw (4). It's fitted with a rubber gasket (5) of 50 mm internal diameter to make a seal against the specimen. Circular specimens are clamped between rubber gaskets over the orifice. Compressed air enters the vessel through a tube (B), thereby forcing air up against the specimen. Tube (B) is also connected to U-tube manometer (D) by means of a valve (C) and the pressure of air against the fabric is the pressure shown on the adjustable scale mounted on one arm of the manometer tube. The air supply for the test is drawn from a reservoir which is itself fed through, a flow control device from a source (Hydrostatic Head Tester) (Figure 5), which may vary between 4 and 20 Ib/in 2. The flow control device is designed to give the required rate of increase of pressure at 10 cm of water per minute, the rate of loading will be within the limits of 10 ± 0.5 cm/min up to the limit of the apparatus. The maximum head attainable is 150 cm of water.

Test Procedure

A circular specimen 6 cm in diameter, is conditioned at $20^{\circ}C \pm 2$ and 65% RH $\pm 2\%$ and then completely immersed and soaked for three minutes in white alcohol. After soaking, mounted on the testing head of the apparatus and the upper fabric surface is covered with white alcohol. The air pressure is raised on the lower surface, at a rate of pressure of 10 cm head of water per minute; this hydrostatic pressure h, in cm of water is then noted. Ten specimens are tested and the equivalent diameter of the third largest pore in the specimen, de, is calculated for each specimen from the formula.

$$d_{e} = \frac{4\gamma}{\rho g h} \times 10^{6}, \text{microns}$$
(17)
Where:

d_e-Equivalent pore diameter, microns

 γ -The surface tension of the white alcohol in newton per meter at the temperature at which the test is carried out (γ =25.9×10⁻³ N/M at 23°C)

h-Hydrostatic pressure in cm of water

g-The acceleration of gravity, is taken as 9.81 m/sec²

p-Density of white alcohol, is taken as 789 kg/ m³.

The mean equivalent pore diameter of ten specimens is then calculated for the fabric.

Pore size distribution

Pore size distribution of all samples was determined using Matlab program software.

Results and Discussion

Pore size and surface porosity results

In this study, pore size, pore opening size distributions and surface porosity of five woven fabrics were determined using a new technique based on image processing operations in order to predict the comfort behavior of fabrics. The values of pore opening sizes based on digital image method were slightly larger than the traditional ones except sample (1A). The percentage of error, i.e., percentage difference between the image pore size and the traditional values, was in a range of 2 to 13 % for the tested woven fabrics. While the difference.

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The image pore size and surface porosity were calculated by a program written in Matlab software.

Then the obtained results were compared with the experimental results. The variations exhibited in pore size and surface porosity for both conventional (traditional) and digital image methods were summarized in Tables 2 and 3, between image porosity and calculated values ranges from 3-11%. Values of pore size of the fabric samples determined by the image method and conventional method are presented in Figure 7 and Table 2. While the values of surface porosity of the five woven fabrics determined by the image method and theoretical method is presented in Figure 8 and Table 3.

Methods of measuring pore size and surface porosity were found. The results from a paired t-test [tcal (pore size)=0.0543, t cal (porosity)=0.06307, t tabular=2.776)] suggest that there is no significant

Fabric code		Difference	
	Image analysis	Experimental method equation (17)	(%)
A 1	102.75	118.7	13.437
B 2	125.75	122.3	-2.8209
C 3	136.5	133.2	-2.4775
D 4	955.75	915.17	-4.4341
E 5	1178	1111.82	-5.9524

 Table 2: Comparison of the pore size determined from the image analysis method and the measured experimental method for various fabrics.

Fabric code	Surfac	Difference (%)			
	lmage analysis	Theoretical method equation (8)	I		
A 1	6.6428	7.5075	11.5178		
B 2	7.8678	8.6515	9.0585		
C 3	9.6090	9.9380	3.3105		
D 4	64.2640	61.8930	-3.8308		
E 5	53.1923	47.5820	-11.7908		

 Table 3: Comparison of the surface porosity determined from image analysis method and the theoretical model for various fabrics.



1-Brass cylindrical vessel; 2 – Specimen; 3 - Clamping ring; 4–Screw;
5-Rubber gasket; B– Tube; C – Valve; D-U- tube manometer.
Figure 8: A schematic diagram of the equivalent pore diameter apparatus.

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difference between the digital image process and the traditional methods for both the pore size and surface porosity. This shows that measurement of both pore size and porosity using the image process method is a viable alternative to using the hydrostatic Head Tester and calculation method of surface porosity.

A comparison between the results of the Matlab program and the traditional (conventional) method for the equivalent porediameter (pore size) and porosity was done.

The comparison proved that the programing technique has close results to the traditional (conventional) method.

Image pore size distribution (PSD) results

In this study, we mainly focused on exploration of interyarn PSD, which could be correlated with value we obtained from image analysis. As expected, there would be only one dominant peak in interyarn PSD of a plain woven fabric. Average pore size modeling results should that for the studied samples, PSD peak should range between 1 and 5 pixcls which corresponds to 46.74 to 344.7 μ m. The tests were performed on four specimens of each fabric. The results are given in Figures 9-13. The nomenclature of Table 4 is as follows: (D min) stands for the average







Figure 10: Comparison of image and calculated surface porosity of woven fabrics.





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pore diameter of the first interval (the smallest pores), (Dmax) stands for the average pore diameter of the last interval (the largest pores), (d_{2}) stands for the average pore diameter of the sample and (ε) stands for the surface porosity of the sample. As expected, the effective pore size is not uniform in all samples, even through all seem to have only one dominant peak representing intervarn pore size distribution. The existence of this peak is consistent with the results from literature [25]. All of these results indicated that individuals samples possessed PSD based on the degree of uniformity of effective pore size in its structure. Considering intervarn pore, the uniformity degree is directly related with the magnitude of dominant peak; the higher the magnitude, the more uniform the fabric. The degree to which a peak is dominant, could be evaluated in several ways, such by the magnitude of absolute or relative area under peak, peak height or half- peak width, and any combination of these. This implies that selection of single parameter is not adequate for predicting uniformity degree. In this study, the group with relative area and relative half-peak width are suggested.

As pointed out earlier, the higher the values of (I) is the more uniform fabric in terms of pore size. Accordingly, five samples could be ranked in terms of uniformity based on (I) values. The ranking of fabric samples from best to worst is B2, A1, C3, D4 and E5 define the degree of uniformity of the dominant peak. Obviously, larger peak height, larger relative area under peak and smaller relative half-peak

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Fabric code	Peak height	Half – peak width (pixels)	Peak area (pixels) (a)	Total area(pixels)(b)	Relative area under peak	Relative half- peak width (Wd)	Uniformity degree
					$Ad = \frac{a}{b}$		$I = \frac{Ad}{Wd}$
A 1	1598.75	5	6970.31	8428.5	0.827	5	0.1654
B 2	2004.25	4	6466.19	8854.9	0.7302	4	0.1826
C 3	1255.25	8	7901.13	9205.5	0.8583	8	0.1073
D 4	364.75	37.5	10258.59	22203.1	0.462	37.5	0.0123
E 5	124.5	175	17900	27265.5	0.6565	175	0.0038

Table 4: Parameters of porosity for all five woven fabrics.

Meas Num	Num A1 (Black)		B2 (white)		C3 (Red)		D4 (Brown)		E5 (Gray)	
	Pore size (µm)	No. of pores								
1	1	1349.25	1	15.75	1	497.75	25	(364.75)*	50	93.25
2	3	(1598.75)*	3	(2004.25)*	3	1078.5	75	127.75	150	(124.50)*
3	5	1349.25	5	1471.75	5	(1255.25)*	125	42.75	250	43.75
4	7	368.5	7	578	7	1004.5	175	15.25	350	17
5	9	118.25	9	181.75	9	677.25	225	16	450	16
6	11	59.5	11	83.75	11	252.75	275	6.75	550	5
7	13	28.25	13	58.5	13	49.25	325	3.75	650	8
8	15	7.75	15	35.25	15	10.25	375	5.5	750	3
9	17	2.75	17	15.25	17	1.5	425	3.5	850	1
10	19	0.75	19	4.25	19	0.25	475	2.5	950	3
11	-	-	21	4.75	-	-	525	2	1050	4
12	-	-	-	-	-	-	575	1.25	1150	1
13	-	-	-	-	-	-	625	1.75	1250	1
14	-	-	-	-	-	-	675	1.25	-	-
15	-	-	-	-	-	-	725	0.25	-	-
16	-	-	-	-	-	-	775	1	-	-
17	-	-	-	-	-	-	825	1	-	-

*Maximum number of pores at peak.

Table 5: Results of pore size distribution by image analysis for fabric sample.

Fabric code	Fabric weight (g/m ²)	Fabric* thickness(mm)	Sett (threads /cm)		Yarn coun	Air permability		
			warp	weft	warp	weft	**(m³/(N.sec))	
A1 (Black)	122.6	0.4	34	28.8	332.19	332.19	0.000875	
					[16 Ne]	[16 Ne] [16 Ne]		
B2 (White)	100.8	0.17	35	30	312.65	265.75	0.001025	
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D4 (Brown)	75.6	0.35	27.6	23.6	88.58	106.3	0.00125	
					[15.3 Ne]	[13.3 Ne]		
E5 (Gray)	131.5	131.5 0.21 16 12		12	265.75	379.64	0.002625	
					[20 Ne]	[14 Ne]		

*Obtained with the "Shirley" thickness meter at a pressure of 70gf/ cm².

**Obtained with the "Shirley" air permeability apparatus, conforming to B.S. Handbook No. 11, P. 308. "Air Permeability of textile Fabrics.

Table 6: Uniformity degree evaluations of image (PSD) profiles by index (I).

width should lead to higher uniformity degree (Table 5).

An index (I) is introduced here to combine these two parameters [26].

$$=\frac{\mathrm{Ad}}{\mathrm{Wd}}$$
(18)

Where: (Ad) is the ratio of area under dominant peak to total area under PSD curve. The value of (Ad) lies in the range 0 to 1.

(Wd) is the ratio of half-peak width to unit width of PSD (I) should, thus, be dimensionless and have a value between 0 to 1. The values of the degree of uniformity of tested samples were evaluated with this index and the results are summarized in Table 6. It should be mentioned that all of these results are based on the average (PSD) of four tests in each sample.

In order to determine whether a relationship exists between the position of the distribution peak and the air permeability for all fabrics studies, the values of air permeability in Table 1 and pore diameter at peak in Table 4 have been plotted in Figures 14-16. Though the points are few and somewhat scattered, there is a definite indication of a correlation.

Conclusion

Experimental results for determination of the pore size of woven

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structures through image analysis are presented. The image analysis method could be used to measure the surface porosity, pore size and size distribution in single layer woven fabrics. The analysis clearly shows that the interstices between warp and weft threads are extremely irregular with respect to size and shape.

The pore size results obtained using digital image processing technique have been validated experimentally and compared with the hydraulic pore diameter measured by Hydrostatic Head Tester. The comparison between the results from the digital measurements of the surface porosity and the theoretically calculated from Equation (8) shows that there may be small differences between these values, except in the case of sample (E). In addition, based upon the digital image results of this study, a standard procedure has been developed and demonstrated for predicting (PSD) in a plain woven fabric. In this procedure, peak height, relative half-peak width relative area under peak and degree of uniformity of effective pore size in the fabric structure are termined from actual measurements derived from image analysis technique. The tested fabric samples could be ranked in a decrease order successfully. A comparison of the peaks of the pore distributions with air permeability data indicates a correlation between the interfibre pore spaces and the air permeability. However, the interyarn porosity may sometimes be a significant factor.

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