

Convergence Control Parameter Region for an Unsteady Three Dimensional Navier-Stokes Equations of Flow between Two Parallel Disks by using Homotopy Analysis Method

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Abstract

Purpose: The paper aims to find the convergence control parameter region for an unsteady three dimensional Navier-Stokes equations of flow between two parallel disks by using Homotopy Analysis Method.

Findings: The region and value of the convergence control parameter has been found.

Keywords: 3D Navier-Stokes equation; Homotopy analysis method; Convergence; System of nonlinear differential equations

Introduction

In mathematics and physics, nonlinear partial differential equations are partial differential equations with nonlinear terms. A few nonlinear differential equations have known exact solutions, but many which are important in applications do not. Sometimes these equations may be linearized by an expansion process in which nonlinear terms are discarded. When nonlinear terms make vital contributions to the solution this cannot be done, but sometimes it is enough to retain a few small ones. Then a perturbation theory may be used to obtain the solution. The differential equations may sometimes be approximated by an equation with small nonlinearities in more than one way, giving rise to different solutions valid over different range of its parameters.

Most scientific and engineering problems are modeled by ordinary differential equations or partial differential equations, Some of them are solved using the analytic methods of perturbation by Nayfeh [1]. In the numerical methods, stability and convergence should be considered so as to avoid divergence or inappropriate results. In the analytic perturbation methods, we should exert the small parameter in the equation. In numerical methods the advantage is that we have to use the small parameter a lot since most problems do not have known analytic solutions, or that if they are known it is too complex to deal with them. The main advantage in analytic method is that it is exact and gives us more context. One of the semi-exact methods which do not need small or large parameters is the Homotopy Analysis Method (HAM), first proposed by Liao in his Ph.D thesis. Liao [2] employed the basic ideas of homotopy in topology to propose a general analytic method for nonlinear problems, namely HAM, which is a powerful analytical method for solving linear and nonlinear differential equations. The HAM also avoids discretization and provides an efficient solution with high accuracy, minimal calculations and avoidance of physically unrealistic assumption. Furthermore, the HAM always provides us with a family of solution expressions with the auxiliary parameter \hbar , the convergence region and the rate of each solution might be determined conveniently by the auxiliary parameter \hbar . HAM contains the homotopy perturbation method (HPM) discussed by He [3], the Adomian decomposition method (ADM) examined by Allan [4], and the d-expansion method.

The main goal of the present study is to find the value of convergence control parameter for the problem of flow between two disks by the HAM.

Mathematical Formulation

Consider the axis-symmetric flow between two infinite disks with a distance d between them. Both disks are placed in the radial direction with a velocity proportional to the radii. The bottom disk is located in the $z = 0$ plane. The velocity ratio of the upper disk to the lower one is γ and ε is the amplitude of the disk. For an incompressible fluid without body forces and based on axis symmetric reads from the papers discussed by Dinarvand [5] and Munnavar [6].

$$\frac{1}{r} \frac{\partial}{\partial r}(ru_r) + \frac{\partial u_z}{\partial z} = 0, \quad (1)$$

$$\frac{\partial u_r}{\partial t} + u_r \frac{\partial u_r}{\partial r} + u_z \frac{\partial u_r}{\partial z} = \nu \left(\frac{\partial^2 u_r}{\partial r^2} + \frac{1}{r} \frac{\partial u_r}{\partial r} + \frac{\partial^2 u_r}{\partial z^2} - \frac{u_r}{r^2} \right), \quad (2)$$

$$\frac{\partial u_z}{\partial t} + u_r \frac{\partial u_z}{\partial r} + u_z \frac{\partial u_z}{\partial z} = \nu \left(\frac{\partial^2 u_z}{\partial r^2} + \frac{1}{r} \frac{\partial u_z}{\partial r} + \frac{\partial^2 u_z}{\partial z^2} \right). \quad (3)$$

Where the velocity vector $\vec{V} = (u_r, u_z)$, ν is the kinematic viscosity. By using von Karman type similarity transformations, similarity functions can be sought as follows,

$$u_r = rF(\eta), \text{ and } u_z = dH(\eta),$$

where $\eta = \frac{z}{d} = \frac{z}{\gamma t}$ is the similarity variable. Substituting the similarity functions into the equations (1), (2) and (3). Therefore, the governing equations yields a similarity equation group

$$\begin{cases} F'' &= Re(F^2 + ReF + 2ReHF + ReH^2F), \\ H' &= -2F. \end{cases} \quad (4)$$

with boundary conditions

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$$F(0) = 1 + \varepsilon \cos t, \quad H(0) = H(1) = 0 \quad \text{and} \quad F(1) = \gamma. \quad (5)$$

Where $Re = \frac{d^2}{\nu}$ is the Reynolds number of the wall and γ is the parameter of the upper disk showing the velocity ratio of the upper disk to the bottom disk. Without loss of generality, we assumed that $0 \leq \gamma \leq 1$.

Analytical solution with HAM

Due to basic idea of HAM, as described in detail by Liao [7,8], according to the boundary conditions (5), we choose

$$F_0(\eta) = 1 - (1 + \varepsilon \cos t - \gamma)\eta + \varepsilon \cos t, \quad (6)$$

$$H_0(\eta) = 0, \quad (7)$$

as initial guesses of $F(\eta)$, and $H(\eta)$ which satisfy the boundary conditions (5). Besides, we select the auxiliary linear operators $\mathcal{L}_1(F)$, and $\mathcal{L}_2(H)$ as

$$\mathcal{L}_1(F) = F'', \quad (8)$$

$$\mathcal{L}_2(H) = H', \quad (9)$$

satisfying the following properties

$$\mathcal{L}_1(c_1\eta + c_2) = 0, \quad (10)$$

$$\mathcal{L}_2(c_3) = 0. \quad (11)$$

Where c_i , $i=1, 2, 3$ are arbitrary constants. If $q \in [0, 1]$ is an embedding parameter and \hbar is an auxiliary nonzero parameter, then the zeroth-order deformation equations are of the following form,

$$(1-q)\mathcal{L}_1[\hat{F}(\eta; q) - F_0(\eta)] = q\hbar\mathcal{N}_1[\hat{H}(\eta; q), \hat{F}(\eta; q)], \quad (12)$$

$$(1-q)\mathcal{L}_2[\hat{H}(\eta; q) - H_0(\eta)] = q\hbar\mathcal{N}_2[\hat{H}(\eta; q), \hat{F}(\eta; q)]. \quad (13)$$

subject to the boundary conditions

$$\hat{F}(0; q) = 1 + \varepsilon \cos t, \quad \hat{F}(1; q) = \gamma,$$

$$\hat{H}(0; q) = \hat{H}(1; q) = 0,$$

in which we define the nonlinear operators \mathcal{N}_1 and \mathcal{N}_2 as

$$\mathcal{N}_1[\hat{H}(\eta; q), \hat{F}(\eta; q)] = \frac{\partial^2 \hat{F}(\eta; q)}{\partial \eta^2} - Re(2Re(\hat{H}(\eta; q))(\hat{F}(\eta; q)) + Re(\hat{F}(\eta; q)))$$

$$+ (\hat{F}(\eta; q))^2 + Re(\hat{H}(\eta; q))^2 (\hat{F}(\eta; q)),$$

$$\mathcal{N}_2[\hat{H}(\eta; q), \hat{F}(\eta; q)] = \frac{\partial \hat{H}(\eta; q)}{\partial \eta} + 2\hat{F}(\eta; q).$$

Clearly, when $q = 0$ the zero-order deformation equations (12) and (13) give rise to:

$$\hat{F}(\eta; 0) = F_0(\eta), \quad \hat{H}(\eta; 0) = H_0(\eta), \quad \hat{P}(\eta; 0) = P_0(\eta). \quad (14)$$

when $q=1$, they become:

$$\hat{F}(\eta; 1) = F(\eta), \quad \hat{H}(\eta; 1) = H(\eta), \quad \hat{P}(\eta; 1) = P(\eta). \quad (15)$$

As q increases from 0 to 1, $\hat{F}(\eta; q)$ and $\hat{H}(\eta; q)$ vary from $F_0(\eta)$ and $H_0(\eta)$ to $F(\eta)$ and $H(\eta)$.

Expanding $\hat{F}(\eta)$ and $\hat{H}(\eta)$ in Maclaurin series with respect to the embedding parameter q and equations (14) and (15), we obtain

$$\hat{F}(\eta; q) = F_0(\eta) + \sum_{m=1}^{+\infty} F_m(\eta)q^m, \quad (16)$$

$$\hat{H}(\eta; q) = H_0(\eta) + \sum_{m=1}^{+\infty} H_m(\eta)q^m, \quad (17)$$

where

$$F_m(\eta) = \frac{1}{m!} \frac{\partial^m \hat{F}(\eta; q)}{\partial q^m} \Big|_{q=0},$$

$$H_m(\eta) = \frac{1}{m!} \frac{\partial^m \hat{H}(\eta; q)}{\partial q^m} \Big|_{q=0}.$$

As pointed by Liao [9], the convergence of the series (16) – (17) strongly depend upon auxiliary parameter \hbar . Assume that \hbar is selected such that the series (16) – (17) are convergent at $q = 1$ then due to equations (14) and (15) we have

$$F(\eta) = F_0(\eta) + \sum_{m=1}^{+\infty} F_m(\eta), \quad (18)$$

$$H(\eta) = H_0(\eta) + \sum_{m=1}^{+\infty} H_m(\eta). \quad (19)$$

Differentiating the zero-order deformation equations (12) and (13) m times with respect to q , then setting $q = 0$ and finally dividing by $m!$ we have the m^{th} - order deformation equations [10-18].

$$\mathcal{L}_1[F_m(\eta) - \chi_m F_{m-1}(\eta)] = \hbar R_{1,m}(\eta), \quad (20)$$

$$\mathcal{L}_2[H_m(\eta) - \chi_m H_{m-1}(\eta)] = \hbar R_{2,m}(\eta). \quad (21)$$

with the following boundary conditions

$$F_m(0) = F_m(1) = 0 \quad \text{and} \quad H_m(0) = H_m(1) = 0, \quad (22)$$

where

$$R_{1,m}(\eta) = \frac{\partial^2 F_{m-1}(\eta)}{\partial \eta^2} - Re \sum_{i=0}^{m-1} (F_i(\eta)F_{m-1-i}(\eta) + Re F_i(\eta))$$

$$+ 2Re H_i(\eta)F_{m-1-i}(\eta) + \sum_{i=0}^i Re H_i(\eta)H_{i-1}(\eta)F_{m-1-i}(\eta),$$

$$R_{2,m}(\eta) = \frac{\partial H_{m-1}(\eta)}{\partial \eta} + 2F_{m-1}(\eta),$$

and

$$\chi_m = \begin{cases} 0 & m \leq 1, \\ 1 & m > 1. \end{cases}$$

Then the solutions for equations (20) and (21) can be expressed by:

$$F_m(\eta) = \chi_m F_{m-1} + \hbar \mathcal{L}_1^{-1}[R_{1,m}] + c_1\eta + c_2,$$

$$H_m(\eta) = \chi_m H_{m-1} + \hbar \mathcal{L}_2^{-1}[R_{2,m}] + c_3.$$

Where c_1, c_2, c_3 are integral constants can be found by boundary conditions (22). For example, we can obtain the following result for solving the first-order deformation equation by using symbolic software *MATHEMATICA*, and successively obtain [19-25],

$$F_1(\eta) = \frac{-1}{24} \hbar(-1+n)Re(9-9n+3n^2+8Re-4nRe+4v+4nv-4n^2v$$

$$+4Rev+4nRev+2V^2+2nv^2+2n^2v^2-4(-3-2Re+n(3+Re-v)$$

$$+n^2(-1+v-v)Cos[t] + (3-3n+n^2)Cos[2t]),$$

$$H_1(\eta) = \hbar(-3+2n+n^2(-1+v)+v-(3-2n+n^2)Cos[t]).$$

Convergence of HAM solution

The totally analytic series solutions of the functions $F(\eta)$ and $H(\eta)$ are given in equations (18) – (1819). The convergence of these series and the rate of approximation for the HAM strongly depends upon the value of the auxiliary parameter \hbar , as pointed out by Liao

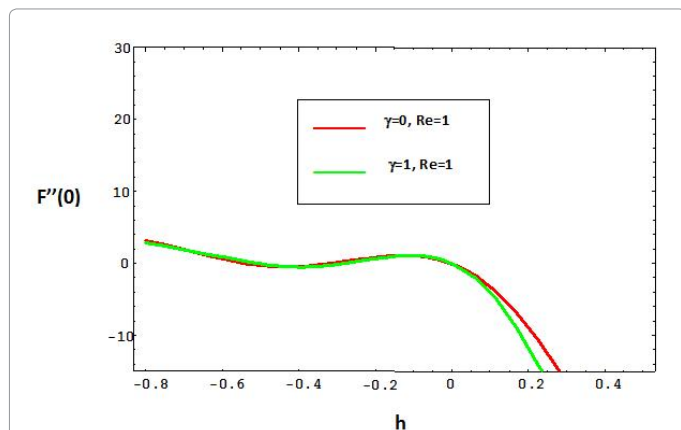


Figure 1: The h – curve of $F''(0)$, obtained by 11th order approximation of the HAM for $\gamma=0$, $\gamma=1$, $\epsilon=1$ and $t=1$ with $Re=1$.

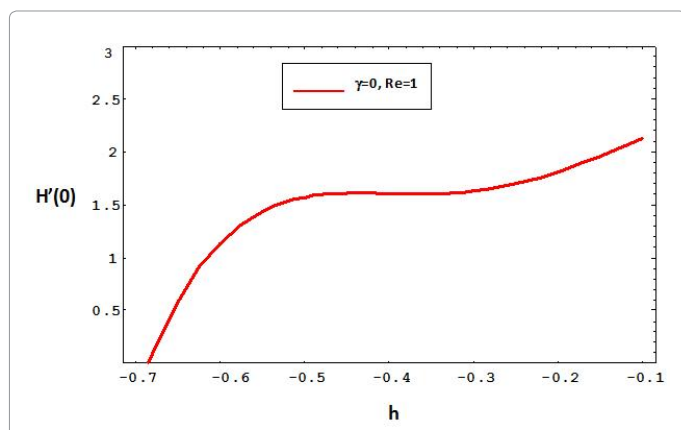


Figure 2: The h – curve of $H'(0)$, obtained by 11th order approximation of the HAM for $\gamma=0$, $\gamma=1$, $\epsilon=1$ and $t=1$ with $Re=1$.

[8]. In general, by means of the h -curve, it is straightforward to choose a proper value of h to control the convergence of the approximation series. To find the range of the admissible values of h , h - curves of $F''(0)$ and $H'(0)$ obtained by the 11th order approximation of the HAM for $\gamma = 0$ and $\gamma = 1$ at $Re = 1$, $t = 1$ and $\epsilon = 1$ are plotted in Figures 1 and 2, respectively. From these figures, the valid regions of h correspond to the line segments nearly parallel to the horizontal axis. Sometimes this region is not perfectly flat to the slowly convergence rate of the series solution which was discussed by Liao in his book Homotopy Analysis Method. However a value of h can be picked up. Therefore in this problem we can choose $h = -0.4$ [26-28].

Conclusion

In this paper, the HAM was used for finding the convergence control parameter of the system of nonlinear ODE derived from von Karman type similarity transform for the unsteady state three dimensional Navier-Stokes equations of flow between two parallel disks. Unlike perturbation methods, the HAM does not depend on any small physical parameters. Thus homotopy analysis method is valid for both weakly and strongly nonlinear problems. Different from all other analytic methods, the homotopy analysis method provides us a simple way to adjust and control the convergence region of the series solution by means of auxiliary parameter h . Thus, the auxiliary parameter h

plays a vital role within the frame of HAM which can be determined by the h curves.

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